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**Building acoustics — Estimation of  
acoustic performance of buildings  
from the performance of elements —**

**Part 4:  
Transmission of indoor sound to the  
outside**

*Acoustique du bâtiment — Calcul de la performance acoustique des  
bâtiments à partir de la performance des éléments —*

*Partie 4: Transmission du bruit intérieur à l'extérieur*



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ISO copyright office  
Ch. de Blandonnet 8 • CP 401  
CH-1214 Vernier, Geneva, Switzerland  
Tel. +41 22 749 01 11  
Fax +41 22 749 09 47  
copyright@iso.org  
www.iso.org

# Contents

Page

<b>Foreword</b>	<b>iv</b>
<b>Introduction</b>	<b>v</b>
<b>1 Scope</b>	<b>1</b>
<b>2 Normative references</b>	<b>1</b>
<b>3 Terms and definitions</b>	<b>1</b>
3.1 Quantities to express building performance	2
3.2 Quantities to express element performance	2
3.3 Other terms and quantities	3
<b>4 Calculation model</b>	<b>3</b>
4.1 General principles	3
4.2 Determination of substitute point sound sources	4
4.3 Determination of the sound power level for a substitute point source	5
4.3.1 General	5
4.3.2 Segment of structural elements of the building envelope	5
4.3.3 Segment of openings	6
4.4 Determination of the directivity correction for a substitute point source	7
4.5 Limitations	7
<b>5 Accuracy</b>	<b>7</b>
<b>Annex A (normative) List of symbols</b>	<b>8</b>
<b>Annex B (informative) Interior sound field</b>	<b>9</b>
<b>Annex C (informative) Sound reduction index</b>	<b>10</b>
<b>Annex D (informative) Directivity of sound radiation</b>	<b>11</b>
<b>Annex E (informative) Simplified model to predict exterior sound pressure levels</b>	<b>12</b>
<b>Annex F (informative) Application of the model to single number ratings</b>	<b>15</b>
<b>Annex G (informative) Calculation example</b>	<b>17</b>
<b>Bibliography</b>	<b>23</b>

## Foreword

ISO (the International Organization for Standardization) is a worldwide federation of national standards bodies (ISO member bodies). The work of preparing International Standards is normally carried out through ISO technical committees. Each member body interested in a subject for which a technical committee has been established has the right to be represented on that committee. International organizations, governmental and non-governmental, in liaison with ISO, also take part in the work. ISO collaborates closely with the International Electrotechnical Commission (IEC) on all matters of electrotechnical standardization.

The procedures used to develop this document and those intended for its further maintenance are described in the ISO/IEC Directives, Part 1. In particular the different approval criteria needed for the different types of ISO documents should be noted. This document was drafted in accordance with the editorial rules of the ISO/IEC Directives, Part 2 (see [www.iso.org/directives](http://www.iso.org/directives)).

Attention is drawn to the possibility that some of the elements of this document may be the subject of patent rights. ISO shall not be held responsible for identifying any or all such patent rights. Details of any patent rights identified during the development of the document will be in the Introduction and/or on the ISO list of patent declarations received (see [www.iso.org/patents](http://www.iso.org/patents)).

Any trade name used in this document is information given for the convenience of users and does not constitute an endorsement.

For an explanation on the meaning of ISO specific terms and expressions related to conformity assessment, as well as information about ISO's adherence to the World Trade Organization (WTO) principles in the Technical Barriers to Trade (TBT) see the following URL: [www.iso.org/iso/foreword.html](http://www.iso.org/iso/foreword.html).

This document was prepared by the European Committee for Standardization (CEN) Technical Committee CEN/TC 126, *Acoustic properties of building elements and of buildings*, in collaboration with ISO Technical Committee TC 43, *Acoustics*, SC 2, *Building acoustics*, in accordance with the agreement on technical cooperation between ISO and CEN (Vienna Agreement).

This first edition cancels and replaces ISO 15712-4:2005, which has been technically revised.

A list of all the parts in the ISO 12354 series can be found on the ISO website.

## Introduction

This document is part of a series specifying calculation models in building acoustics.

Although this document covers the main types of building construction it cannot as yet cover all variations in the construction of buildings. It sets out an approach for gaining experience for future improvements and developments.

The accuracy of this document alone is difficult to specify since it forms just one link in the chain of inside sound level, sound radiation and sound propagation outdoors; the first and last item are not covered by this document. The accuracy can only be specified after widespread comparisons with field data in combination with other prediction standards, i.e. those for outdoor sound propagation. It is the responsibility of the user (i.e. a person, an organization, the authorities) to address the consequences of the accuracy, inherent for all measurement and prediction methods, by specifying requirements for the input data and/or applying a safety margin to the results or applying some other correction.

It is intended for acoustical experts and provides the framework for the development of application documents and tools for other users in the field of building construction, taking into account local circumstances.

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# Building acoustics — Estimation of acoustic performance of buildings from the performance of elements —

## Part 4: Transmission of indoor sound to the outside

### 1 Scope

This document specifies a calculation model to estimate the sound power level radiated by the envelope of a building due to airborne sound inside that building, primarily by means of measured sound pressure levels inside the building and measured data which characterize the sound transmission by the relevant elements and openings in the building envelope. These sound power levels, together with those of other sound sources in or in front of the building envelope, form the basis for the calculation of the sound pressure level at a chosen distance from a building as a measure for the acoustic performance of buildings.

The prediction of the inside sound pressure level from knowledge of the indoor sound sources is outside the scope of this document.

The prediction of the outdoor sound propagation is outside the scope of this document.

NOTE For simple propagation conditions an approach is given for the estimation of the sound pressure level in [Annex E](#).

This document describes the principles of the calculation model, lists the relevant quantities and defines its applications and restrictions.

### 2 Normative references

The following documents are referred to in the text in such a way that some or all of their content constitutes requirements of this document. For dated references, only the edition cited applies. For undated references, the latest edition of the referenced document (including any amendments) applies.

ISO 7235, *Acoustics — Laboratory measurement procedures for ducted silencers and air-terminal units — Insertion loss, flow noise and total pressure loss*

ISO 10140-1:2016, *Acoustics — Laboratory measurement of sound insulation of building elements — Part 1: Application rules for specific products*

ISO 16283-3, *Acoustics — Field measurement of sound insulation in buildings and of building elements — Part 3: Airborne sound insulation of façades*

### 3 Terms and definitions

For the purposes of this document, the following terms and definitions, and the symbols and units listed in [Annex A](#), apply.

ISO and IEC maintain terminological databases for use in standardization at the following addresses:

- IEC Electropedia: available at <http://www.electropedia.org/>
- ISO Online browsing platform: available at <http://www.iso.org/obp>

### 3.1 Quantities to express building performance

#### 3.1.1

##### sound power level

$L_W$

sound power level of a substitute point sound source

#### 3.1.2

##### directivity correction

$D_c$

deviation in decibels between the sound pressure level of a point sound source in a specified direction and the level of an omni-directional point source producing the same sound power level

### 3.2 Quantities to express element performance

NOTE For the calculations, additional information on constructions could be necessary; for example, the shape of the building envelope, areas, etc.

#### 3.2.1

##### sound reduction index

$R$

ten times the common logarithm of the ratio of the sound power  $W_1$  incident on a test specimen to the sound power  $W_2$  transmitted through the specimen, which is evaluated from

$$R = \left( 10 \lg \frac{W_1}{W_2} \right) \text{ dB}$$

Note 1 to entry: This quantity shall be determined in accordance with ISO 10140-1:2016, Annexes A, B, C and D or ISO 16283-1.

#### 3.2.2

##### element normalized level difference

$D_{n,e}$

difference in the space and time average sound pressure level produced in two rooms by a source in one room, where sound transmission is only due to a small technical element (e.g. transfer air devices, electrical cable ducts, transit sealing systems), which is evaluated from

$$D_{n,e} = L_1 - L_2 - \left( 10 \lg \left( \frac{A}{A_0} \right) \right) \text{ dB}$$

where  $A$  is the equivalent sound absorption area in the receiving room, in square metres.

Note 1 to entry:  $D_{n,e}$  is normalized to the reference equivalent sound absorption area ( $A_0$ ) in the receiving room;  $A_0 = 10 \text{ m}^2$ .

Note 2 to entry: This quantity shall be determined in accordance with ISO 10140-1:2016, Annex E.

#### 3.2.3

##### insertion loss

$D$

<of an element> reduction in sound power level at a given location behind the element due to the insertion of the element into the duct in place of a hard-walled duct section

Note 1 to entry: This quantity shall be determined in accordance with ISO 7235.

Note 2 to entry: For elements where this document does not apply equivalent methods should be used.



### 3.3 Other terms and quantities

#### 3.3.1

##### sound pressure level

$L_p$

measure of sound at a specified reception point outside a building, due to the sound produced inside the building and by sources associated with the building as normally determined by measurements according to local requirements (specifying relevant positions, integration period and source conditions)

Note 1 to entry: The sound pressure level is normally A-weighted.

#### 3.3.2

##### total attenuation due to propagation

$A_{\text{tot}}$

level difference between the radiated sound power and the sound pressure at a position at distance  $d$  from the building envelope due to the total of all propagation effects

Note 1 to entry: Propagation effects include geometrical divergence, air absorption, ground effect, screening, etc.

#### 3.3.3

##### diffusivity term

$C_d$

level difference between the sound pressure level at 1 m to 2 m from the inside face of the relevant building element and the intensity level of the incident sound perpendicular to that element

Note 1 to entry: For a diffuse field and reflecting walls, the diffusivity term is  $C_d = -6$  dB; for other situations it can have a value between 0 dB and  $-6$  dB.

#### 3.3.4

##### inside sound pressure level

$L_{p,\text{in}}$

sound pressure level inside the building, 1 m to 2 m from the considered element or segment of the building envelope

Note 1 to entry: In the case of a diffuse sound field, this corresponds to the average sound pressure level in the diffuse sound field.

#### 3.3.5

##### substitute point source

point source for which the radiated sound is the same as that of a segment of the building envelope

Note 1 to entry: The segment can be composed of one or more building elements or of one or more openings.

## 4 Calculation model

### 4.1 General principles

The total sound pressure level at a reception point that is a chosen distance from a building is determined by the following contributions:

- the sound radiated by the elements of the building envelope due to the sound pressure level inside;
- the sound radiated by individual sound sources, fixed in or onto the outside of the building;
- the outdoor sound propagation (effects of distance, air absorption, ground effect, screening, reflections, etc.).

The sound radiation by the building envelope may be represented by the radiation of one or more substitute point sources. Each point source can represent the contribution of a segment of the building envelope or a group of individual sound sources. The number of point sources required to adequately

represent a building depends upon the distance of each reception point from the building and the variation in propagation effects. Normally, the building envelope is represented by at least one point source for each side, i.e. walls and roofs, but often several point sources are required for each side.

The sound pressure level at a reception point outside the building is determined from the contributions of each substitute point source according to [Formula \(1\)](#):

$$L_p = L_W + D_c - A_{\text{tot}} \quad (1)$$

where

$L_p$  is the sound pressure level at a reception point outside the building due to the sound radiation of a substitute point source, in decibels;

$L_W$  is the sound power level of the substitute point source, in decibels;

$D_c$  is the directivity correction for the substitute point sources in the direction of the reception point, in decibels;

$A_{\text{tot}}$  is the total attenuation that occurs during sound propagation from the substitute point source to the reception point, in decibels.

The calculation model described in this document is restricted to the calculation of the sound power level of the substitute point sources for the building elements and openings in the building envelope from data on

- the inside sound pressure level, and
- the elements which form the building envelope.

The model also gives indications of the directivity correction that can be expected for various types of elements. The inside sound pressure level will normally be the equivalent sound pressure level over a specified period according to the relevant requirements. However, other types of levels can also be used, for instance the maximum level. The calculation of the inside sound pressure level is outside the scope of this document.

The calculation of the contribution of individual sound sources is outside the scope of this document.

The total attenuation  $A_{\text{tot}}$  due to propagation effects, necessary for the prediction of the sound pressure level at the reception point, can be estimated according to available methods for outdoor propagation, based on a point source approach. The calculation of these propagation effects is outside the scope of this document.

NOTE One such method is given in ISO 9613-2, where the total attenuation is indicated as  $A$ . The total attenuation follows from the addition of the attenuation due to various propagation effects, such as geometrical divergence, air absorption, ground effect, screening, etc.

However, for simple propagation conditions an approach is given for the estimation of the sound pressure level in [Annex E](#).

A calculation example is given in [Annex G](#).

## 4.2 Determination of substitute point sound sources

The elements contributing to the sound radiation are divided into two groups:

- plane radiators, such as structural elements of the building envelope, i.e. walls, roof, windows, doors, including small building elements with an area of typically less than 1 m<sup>2</sup>, such as grids and openings;

- larger openings, area typically 1 m<sup>2</sup> or more, i.e. large ventilation openings, open doors, open windows.

To calculate the sound propagation outside the building each element can be represented by a substitute point sound source. However, the building may also be divided into larger segments which are each represented by a substitute point sound source. For the segmentation the following rules apply:

- the sound propagation to the nearest reception points of interest ( $A_{tot}$ ) is the same for all elements of a segment;
- the distance to the nearest reception point of interest is larger than twice the largest dimension of the segment;
- for the elements in a segment the same inside sound pressure level is applicable;
- for the elements in a segment the same directivity is applicable.

If one or more of these conditions is not fulfilled, choose different segments for instance smaller segments, until these conditions are met.

Unless otherwise specified in the propagation model, the point source representing a vertical segment is positioned at half the width of the segment and 2/3 the height of the segment; for all other segments the position is at the centroid of the segment.

### 4.3 Determination of the sound power level for a substitute point source

#### 4.3.1 General

For each segment the sound power level is determined from the following input data:

- sound pressure level inside:  $L_{p,in}$ ;
- sound reduction index of large building element  $i$  of the building envelope:  $R_i$ ;
- element normalized level difference of small element  $i$ :  $D_{n,e,i}$ ;
- insertion loss of silencing element for opening  $i$ :  $D_i$ ;
- area of building element or opening  $i$ :  $S_i$ .

#### 4.3.2 Segment of structural elements of the building envelope

The sound power level for the substitute point source is determined by [Formula \(2\)](#):

$$L_W = L_{p,in} + C_d - R' + 10 \lg \frac{S}{S_0} \quad (2)$$

where

$L_{p,in}$  is the sound pressure level at 1 m to 2 m from the inside of the segment, in decibels;

$C_d$  is the diffusivity term for the inside sound field at the segment, in decibels;

$R'$  is the apparent sound reduction index for the segment, in decibels;

$S$  is the area of the segment, in square metres;

$S_0$  is the reference area, in square metres ;  $S_0 = 1 \text{ m}^2$ .

The apparent sound reduction index for the segment follows from the data on the composing elements  $i$  by [Formula \(3\)](#):

$$R' = -10 \lg \left( \sum_{i=1}^m \frac{S_i}{S} 10^{-R_i/10} + \sum_{i=m+1}^{m+n} \frac{A_o}{S} 10^{-D_{n,e,i}/10} \right) \quad (3)$$

where

$R_i$  is the sound reduction index of element  $i$ , in decibels;

$S_i$  is the area of element  $i$ , in square metres;

$D_{n,e,i}$  is the element normalized sound level difference for a small element  $i$ , in decibels;

$A_o$  is the reference absorption area, in square metres;  $A_o = 10 \text{ m}^2$ ;

$m$  is the number of large elements of the segment;

$n$  is the number of small elements of the segment.

Information on the inside sound pressure level and diffusivity of the sound field is given in [Annex B](#), based on the type of enclosed space and internal conditions for the elements of the building envelope.

NOTE 1 In the case of an ideal diffuse sound field and non-absorbing elements  $C_d = -6 \text{ dB}$ ; for industrial spaces and segments which are non-absorbing at the inside a value of  $C_d = -5 \text{ dB}$  is generally more appropriate.

NOTE 2 The contribution of structure-borne sound to the sound radiation is not incorporated into the model. It could roughly be incorporated through an adjusted sound reduction index; some indications are given in [Annex C](#).

Information on the sound reduction index to be used is given in [Annex C](#).

### 4.3.3 Segment of openings

The sound power level for the substitute point source is determined by [Formula \(4\)](#):

$$L_W = L_{p,in} + C_d + 10 \lg \sum_{i=1}^o \frac{S_i}{S_o} 10^{-D_i/10} \quad (4)$$

where

$S_i$  is the area of opening  $i$ , in square metres;

$D_i$  is the insertion loss for a silencing element for opening  $i$ , in decibels;

$o$  is the number of openings of the segment.

The calculation of the sound power level is performed in frequency bands, based on acoustic data for the elements in frequency bands (one-third-octave bands or octave bands). The calculation is performed at least for the octave bands from 125 Hz to 2 000 Hz or for the one-third-octave bands from 100 Hz to 3 150 Hz. The calculations can be extended to higher or lower frequencies if acoustic data are available for such a larger frequency range. Information of airborne sound insulation in the low frequency range down to 50 Hz can be found in ISO 12354-1:2017, Annex I. The issues of field measurement of façade sound insulation in the low frequency range are specifically considered in ISO 16283-3.

NOTE For rough indications it could be sufficient to apply the model directly to A-weighted levels and single number ratings of the performance of building elements in accordance with ISO 717-1. Guidelines are given in [Annex F](#).

#### 4.4 Determination of the directivity correction for a substitute point source

The directivity correction  $D_c$  contains the inherent directivity of the radiating elements and openings as given by the directivity index  $D_I$ . It can also contain the effect of the vicinity of hard surfaces (reflection and screening) as given by the solid angle index  $D_\Omega$ .

For a specific direction the directivity correction is determined from [Formula \(5\)](#):

$$D_c = D_I + D_\Omega = D_I + 10 \lg \frac{4\pi}{\Omega} \quad (5)$$

where

$D_I$  is the directivity index, in decibels.

$D_\Omega$  is the solid angle index, in decibels.

$\Omega$  is the solid angle into which radiation occurs, in steradians.

Whether or not the solid angle index is included in the directivity correction depends on the propagation model used. When reflections on the ground and other surfaces are taken into account by image sources, the solid angle index  $D_\Omega = 0$  dB. However, when the reflecting surfaces are the building envelope itself, it is recommended to include the effect of these surfaces in the solid angle index. In giving the directivity correction the value of the included solid angle index is therefore to be stated clearly.

Information on the directivity correction is given in [Annex D](#).

#### 4.5 Limitations

Although large, homogeneous building elements, e.g. a complete side wall, can have specific radiation patterns, favouring certain directions; these effects are not taken into account in the model.

The possible contribution of structure-borne sound by machinery in the building is not included in the model, although an approximate approach is indicated in [Annex C](#).

### 5 Accuracy

The accuracy of the prediction by the model presented depends on many factors: the accuracy of the input data, the fitting of the situation into the model, the type of elements involved, the geometry of the situation, the type of quantity to be predicted and the workmanship. It is therefore not possible to specify the accuracy in general for all types of situations and applications. Data on the accuracy will have to be gathered in the future by comparing the results of the model with a variety of field situations.

In applying the predictions it is advisable to vary the input data, especially in complicated situations and with rare elements with questionable input data. The resulting variation in the results gives an impression of the expected accuracy for these situations assuming similar workmanship.

## Annex A (normative)

### List of symbols

**Table A.1 — List of symbols**

Symbol	Physical quantity	Unit
$A_0$	reference absorption area; $A_0 = 10 \text{ m}^2$	$\text{m}^2$
$A_{\text{tot}}$	total attenuation due to the outside sound propagation from a point source	dB
$A'_{\text{tot},j}$	estimated total attenuation due to the outside propagation in a simple propagation situation for a side of the building	dB
$C_d$	diffusivity term for the inside sound field at a segment or side	dB
$c_0$	speed of sound in air (approximately 340 m/s)	m/s
$D_c$	directivity correction for a substitute point source	dB
$D_l$	directivity index of a substitute point source	dB
$D_\Omega$	solid angle index of a substitute point source	dB
$D_{n,e,i}$	element normalized sound level difference for a small element i	dB
$D_i$	insertion loss for a silencing element for opening i	dB
$d$	distance from the centre of a side of the building to the reception point	m
$d_\perp$	perpendicular distance from the reception point to a side	m
$d_0$	reference distance; $d_0 = 1 \text{ m}$	m
$f$	frequency	Hz
$h_1, h_2$	vertical distances to the two borders of a side from the projection of the reception point on the side	m
$i$	index for element or opening for a segment of the building	-
$j$	index for a segment or side of the building	-
$l_1, l_2$	horizontal distances to the two borders of a side from the projection of the reception point on the side	m
$L_{p,d}$	sound pressure level at a reception point at distance $d$ at the outside the building	dB re 20 $\mu\text{Pa}$
$L_{p,in}$	sound pressure level at 1 m to 2 m from the inside of a segment or side	dB re 20 $\mu\text{Pa}$
$L_W$	sound power level of a substitute point sound source	dB re 1 pW
$m$	number of large elements of segment or side j	-
$n$	number of small elements of segment or side j	-
$o$	number of openings of segment or side j	-
$R_i$	sound reduction index of element i	dB
$R'$	apparent sound reduction index for a segment or side	dB
$S_i$	area of element or opening i	$\text{m}^2$
$S$	area of a segment or side	$\text{m}^2$
$S_0$	reference area; $S_0 = 1 \text{ m}^2$	$\text{m}^2$
$\phi$	angle between the orientation of a substitute point sound source and the direction from this source to the reception	°
$\Omega$	solid angle into which radiation occurs	sr

## Annex B (informative)

### Interior sound field

The inside sound pressure level, relevant for the predictions of sound radiation, is the sound pressure level at a distance of 1 m to 2 m from the interior of the building envelope. It is considered as input data for the model described in this document. This level could be based on measurements in the actual situation, measurements in similar situations or calculations, for instance by empirical models, image source models or ray-tracing models.

The diffusivity term  $C_d$  is influenced by the amount of diffusivity of the interior sound field and the inside absorption of the considered segment of the building envelope. Indications of its value for different rooms are given in [Table B.1](#).

**Table B.1 — Indication of the diffusivity term for different rooms, based on a general description of the spaces and local surface properties of the inside of the building envelope**

Situation	$C_d$ dB
Relatively small, uniformly shaped rooms (diffuse field); in front of reflecting surface	-6
Relatively small, uniformly shaped rooms (diffuse field); in front of absorbing surface	-3
Large flat or long halls, many sources (average industrial building); in front of reflecting surface	-5
Industrial building, few dominating directional sources; in front of reflecting surface	-3
Industrial building, few dominating directional sources; in front of absorbing surface	0

## **Annex C** **(informative)**

### **Sound reduction index**

The sound reduction index of elements can be obtained from laboratory measurements in accordance with ISO 10140-2 and field measurements of sound insulation of façades in accordance with ISO 16283-3. Some information on the sound reduction index according to these documents is also given in ISO 12354-1 and ISO 12354-3.

However, the dimensions of the elements and the mounting methods are generally quite different from those used for laboratory measurements. This can give rise to large deviations between the acoustic data for elements from the laboratory and the apparent values in the actual situation. Moreover, the sound reduction index of composed parts is normally limited by the sound transmission through connections between elements, sealing of slits and small openings. This transmission is difficult to predict and normally not well represented by laboratory measurements. For these reasons it is strongly recommended to apply data based on representative field measurements. If laboratory data are used it is recommended to limit the resulting sound reduction index for a segment in each frequency band to a practical maximum, relevant for the type of constructions and the situation considered.

Direct excitation of the building structures by internal sources causes structure-borne sound transmission through the building which could contribute to the sound radiation. Estimations of this contribution can be performed in accordance with the relevant clauses of EN 12354-5.



## Annex D (informative)

### Directivity of sound radiation

#### D.1 General

Large homogeneous constructions show a directionality for frequencies above the critical frequency, resulting overall in a higher sound radiation parallel to the plane than perpendicular. However, due to inhomogeneities in practical constructions and leakages this is normally not very important. Large plane constructions radiate sound essentially only into a half sphere, so the solid angle into which radiation occurs is  $\Omega = 2 \pi$  leading to  $D_c = +3$  dB. In practice the directivity correction in front of a plane varies between  $D_c = +5$  dB and  $D_c = -5$  dB. It may be taken on average as  $D_c = 0$  dB for radiation angles between  $0^\circ$  and  $90^\circ$  relative to the normal on the plane.

#### D.2 Openings

Openings show in general a radiation pattern with predominance towards the front. The directivity index roughly varies between  $D_I = +2$  dB and  $D_I = -10$  dB. If the opening is silenced (absorbing muffler, lined ducts) the radiation towards the front can be even more pronounced.

If an opening is positioned in a plane or at short distance (less than one wavelength) from one or more reflecting surfaces, the effect of these planes can be incorporated in the directivity correction by considering the solid angle to which radiation is restricted. If the opening is at large distance from a plane, i.e. at the end of a duct protruding through the plane, the radiation will be in all directions and the directivity correction should contain just the directivity index of the opening, the plane being treated as a reflecting object in the propagation model.

## Annex E (informative)

### Simplified model to predict exterior sound pressure levels

The simplified model avoids the need to construct an array of equivalent point sources by presenting the result of the array calculation under certain restriction, leading directly to the outside sound pressure level as radiated by a side of the building. This applies to the following situations:

- the same inside sound pressure level applies for the whole relevant part of the side of the building;
- the distance to the reception point is relatively short;
- the distance to the reception point from large openings is large compared to their dimensions;
- no contribution from individual sound sources is considered;
- no screening exists between the building envelope and the reception point;
- the ground surface is mainly hard.

The distance to the side of the building may be small compared to the dimensions of the building but shall not be large enough for substantial meteorological effects (approximately less than 100 m) or for substantial contributions from radiation by other building sides. This last assumption normally holds true as long as the sound power level of the other side of the building is not substantially larger than that of the considered side.

It is assumed that the considered side of the building envelope radiates uniformly over the area, giving a total sound power level. By representing the side by several identical point sources, the attenuation due to geometrical divergence of the envelope as a whole can then be obtained from the attenuation by geometrical divergence for a point source, by summation over all these point sources taking a density of point sources which is sufficient for the considered distance. Together with the radiation of the side of the building into a quarter sphere formed by the side of the building itself and the hard ground, this gives one expression for the total attenuation, indicated for this simplified model as the estimated total attenuation  $A'_{\text{tot}}$ .

By assuming radiation into a quarter sphere, leading to a contribution to the directivity correction of +6 dB in front of a side of the building, the resulting sound pressure levels are normally on the safe side. In the cases where the ground between the building and reception point is essentially absorbing, the sound pressure level will be over-estimated by at most a few decibels.

The resulting sound pressure at a reception point in front of a side of the building follows from [Formula \(E.1\)](#):

$$L_p = 10 \lg \left( 10^{L_{W,e}/10} + 10^{L_{W,o}} \right) - A'_{\text{tot}} \quad (\text{E.1})$$

where

$L_{W,e}$  is the sound power level for the whole side of the building envelope, in decibels;

$L_{W,o}$  is the sound power level for the (group of) openings in the side of the building, in decibels;

$A'_{\text{tot}}$  is the estimated total attenuation for the simplified propagation for the side of the building, due to geometrical divergence, directivity and ground effect, in decibels.

The sound power level for the considered side of the building envelope as a whole and for the considered total group of openings is determined according to 4.3.

For reception points in front of the considered side of the building the estimated total attenuation follows from Formula (E.2) (see Figure E.1):

$$A'_{\text{tot}} = -10 \lg \frac{S_o}{\pi S} \left( \tan^{-1} \frac{l_1}{d_{\perp}} + \tan^{-1} \frac{l_2}{d_{\perp}} \right) \left( \tan^{-1} \frac{h_1}{d_{\perp}} + \tan^{-1} \frac{h_2}{d_{\perp}} \right) \quad (\text{E.2})$$

where

- $d_{\perp}$  is the perpendicular distance from the reception point to the plane of the side, in metres;
- $S$  is the area of the side of the building, in square metres;
- $S_o$  is the reference area, in square metres;  $S_o = 1 \text{ m}^2$ ;
- $l_1, l_2$  are the horizontal distances to the two borders of the side from the projection of the reception point on the side, in metres;
- $h_1, h_2$  are the vertical distances to the two borders of the side from the projection of the reception point on the side, in metres.

NOTE 1 In deducing this equation from the radiation of point sources an approximation has been used for large distances compared with the dimensions of the radiating side. However, for shorter distances this leads to values which have been shown to be more realistic than making a correct deduction; this is due to the actual directivity of a radiating side.

NOTE 2 For a reception point in front of the centre of the side ( $d = d_{\perp}, l_1 = l_2, h_1 = h_2$ ) the relation simplifies to

$$A'_{\text{tot}} = -10 \lg \frac{4S_o}{\pi S} \tan^{-1} \frac{L}{2d} \tan^{-1} \frac{H}{2d}$$

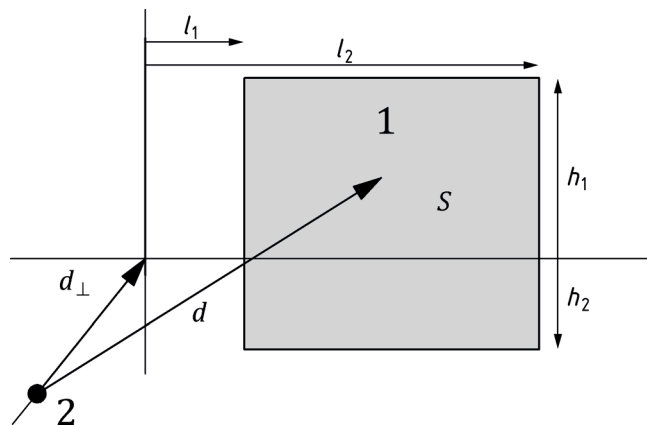
where

- $L$  is the width ( $= 2 l_1 = 2 l_2$ );
- $H$  is the height of the radiating area in metres; ( $S = L H$ ).

NOTE 3 At a distance that is larger than the largest dimension of the side the attenuation term becomes simply

$$A'_{\text{tot}} = -10 \lg \frac{S_o}{\pi d^2}$$

where  $d$  is the distance to the centre of the plane in metres.

**Key**

- 1 building side
- 2 reception point

**Figure E.1 — Illustration of the geometric situation of a radiating side of a building and a reception point**

If the projection of the reception point is outside the radiating area  $S$ , the smallest  $l$  and/or  $h$  is taken as negative, i.e. the corresponding  $\tan^{-1}$ -term is subtracted from the other, otherwise both distances  $l$  and/or  $h$  are taken positive.

The sound pressure level at a distance significantly less than the dimensions of the side, can differ locally from the calculated average level if the sound reduction indices of the composite parts differ significantly or the distance to openings and sources is too small.

Since the attenuation term is independent of frequency, the calculations can also be performed directly for the A-weighted sound pressure level using the A-weighted sound power levels.

NOTE 4 In the case of a reception point at very short distance, e.g. at 1 m, from a part of the building envelope, and assuming that this distance is also small compared to the height above the ground, the [Formulae \(2\)](#), [\(E.1\)](#) and [\(E.2\)](#) are adjusted so as to neglect the ground reflection and simplify to

$$L_{p,d=1m} = L_{p,in} + C_d - R' + 4$$

This relation can be used to estimate the *in situ* apparent sound reduction index of that part of the building envelope from field measurements.

## Annex F (informative)

### Application of the model to single number ratings

#### F.1 General

In some cases only the A-weighted sound pressure level inside the building and the weighted performance of the elements forming the building envelope are known. The following guidelines can be applied in those cases to determine a rough estimate of the A-weighted sound power levels as in 4.3.

#### F.2 Input data

The input data to consider are the following:

- the A-weighted sound pressure level  $L_{pA,in}$  in dB inside the building;
- the weighted airborne sound insulation index  $R_w$  and the spectrum adaption terms  $C$  and  $C_{tr}$  in accordance with ISO 717-1 of the large elements of the building envelope;
- the weighted element normalized level difference  $D_{n,e,w}$  and the spectrum adaption terms  $C$  and  $C_{tr}$  in accordance with ISO 717-1 of the small elements of the building envelope.

#### F.3 Model for single number ratings

The A-weighted sound power level  $L_{WA}$  radiated by a segment of structural elements of the building envelope is estimated in accordance with [Formula \(F.1\)](#):

$$L_{WA} = L_{pA,in} - 6 - X'_{As} + 10 \lg \frac{S}{S_0} \quad (F.1)$$

where

$L_{pA,in}$  is the A-weighted sound pressure level at 1 m to 2 m from the inside of segment j, in decibels;

$X'_{As}$  is the quantity characterizing the A-weighted sound level difference over segment j for source spectrum s, in decibels;

$S$  is the area of segment j, in square metres;

$S_0$  is the reference area, in square metres;  $S_0 = 1 \text{ m}^2$ .

NOTE In several countries  $X'_{A1}$  is indicated as the apparent weighted sound reduction index  $R'_A$  and  $X'_{A2}$  as the apparent weighted sound reduction index  $R'_{Atr}$ .

The characterization of the A-weighted sound level difference for the segment follows from the data on the composing elements i by [Formula \(F.2\)](#):

$$X'_{As} = -10 \lg \left( \sum_{i=1}^m \frac{S_i}{S} 10^{-(R_{w,i} + C_{s,i})/10} + \sum_{i=1}^m \frac{A_o}{S} 10^{-(D_{n,e,w,1} + C_{s,i})/10} \right) \quad (F.2)$$

where

- $R_{w,i}$  is the weighted sound reduction index of element  $i$ , in decibels;
- $D_{n,e,w,i}$  is the weighted element normalized level difference of a small element  $i$ , in decibels;
- $C_{s,i}$  is the spectrum adaptation term for spectrum  $s$  of element  $i$ , in decibels;
- $S_i$  is the area of element  $i$ , in square metres;
- $A_0$  is the reference absorption area, in square metres;  $A_0 = 10 \text{ m}^2$ ;
- $m$  is the number of large elements of the segment;
- $n$  is the number of small elements of the segment.

In ISO 717-1 the spectrum  $s = 1$  refers to A-weighted pink noise, the spectrum adaptation term being denoted as  $C$ ; this spectrum is also relevant for factory noise with mainly medium and high frequency sound (ISO 717-1:2013, Annex A). The spectrum  $s = 2$  refers to A-weighted road traffic noise, the spectrum adaptation term being denoted as  $C_{tr}$ ; this spectrum is also relevant for factory noise with mainly low and medium frequency sound and for disco music.

#### F.4 Limitations

Since the procedure for evaluating the single number rating of sound reduction index assumes an interior spectrum with an emphasis on either the high frequencies or the lower frequencies, the accuracy of estimated A-weighted sound power level depends on the agreement between the shapes of the actual interior sound spectrum and the chosen fixed spectrum in accordance with ISO 717-1. The A-weighted sound power level can still be underestimated for sound spectra with main components at frequencies around and below about 250 Hz.

The interior sound field should be diffuse. This condition is fulfilled in enclosed spaces with relatively uniform shape and low sound absorption.

## Annex G (informative)

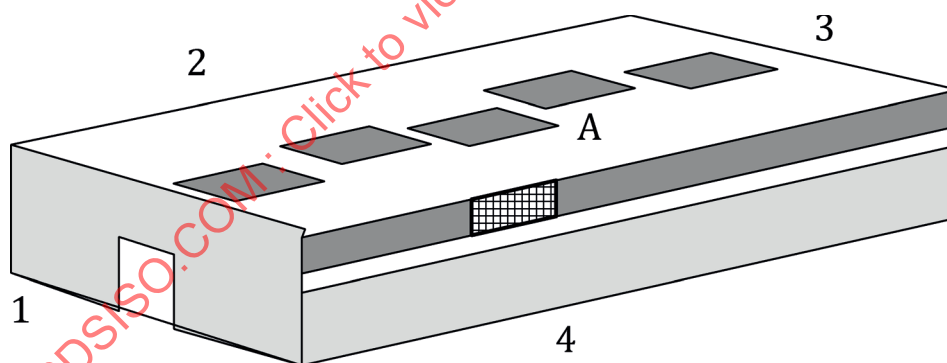
### Calculation example

#### G.1 Situation

##### G.1.1 General

Industrial building, width 60 m, length 100 m, height 10 m (see [Figure G.1](#)).

- |                       |  |
|-----------------------|--|
| Side 1, 10 m × 60 m:  | 100 mm light concrete with a large industrial door, 6 m × 4 m.                                     |
| Side 2, 10 m × 100 m: | 100 mm light concrete with glazing over the whole length; height 1 m, 4 mm glass, partly openable. |
| Side 3, 10 m × 60 m:  | 100 mm light concrete with a small door, 1 m × 2 m.  |
| Side 4, 10 m × 100 m: | as side 2, with silenced ventilation opening (gross 1 m × 4 m).                                    |
| Side 5, 60 m × 100 m: | lightweight metal roof, with 5 glazed light openings (2 m × 2 m) on the centre line.               |



**Key**

- 1, 2, 3, 4 building sides  
A roof

**Figure G.1 — Illustration of a building as example**

The sound pressure level near the walls and roof is the same and given in [Table G.1](#).

The acoustic performance of the building elements is given in [Table G.2](#).

None of the walls or the roof has internal absorbing lining. The minimum distance for reception points of interest is 50 m from the sides of the building.

**Table G.1 — Inside sound pressure level in octave bands**

Level	Octave bands (Hz)							
	63	125	250	500	1 k	2 k	4 k	8 k
$L_{p,in}$ dB re 20 $\mu$ Pa	70	74	76	72	70	67	62	57

### G.1.2 Acoustic data for elements

**Table G.2 — Acoustic data for the building elements, as input to the calculations**

Element	Quantity dB	Octave bands with mid frequency in Hz							
		63	125	250	500	1 k	2 k	4 k	8 k
100 mm light concrete	$R^a$	32	36	36	33	39	49	57	63
4 mm glass windows	$R^a$	15	19	23	25	25	25	25	25
Industrial door	$R^b$	21	23	28	30	30	30	30	30
Normal door	$R^b$	13	17	22	25	25	25	25	25
Roof construction	$R^b$	16	24	27	30	37	44	47	49
Roof glass elements	$R^b$	9	11	15	22	26	30	30	30
Ventilation silencers	$D^a$	0	4	11	13	10	8	8	5
<sup>a</sup> Data from laboratory measurements.									
<sup>b</sup> Data from field measurements.									

## G.2 Results complete model

### G.2.1 Substitute point sources

Minimum distance  $d = 50$  m, thus maximum dimension segments are as follows (see [Figure G.2](#)):

- wall segment =  $1/4 \sqrt{2} d = 17,7$  m, thus segments of  $10 \text{ m} \times 20 \text{ m}$ ;
- roof segment =  $1/4 \sqrt{2} (d + 30) = 28,3$  m, thus segments of  $20 \text{ m} \times 20 \text{ m}$ ;
- Side 1: 3 substitute point sources;  $j = 1$  with door,  $j = 2,3$  without door;
- Side 2: 5 substitute point sources;  $j = 1$  to 5, all identical;
- Side 3: 3 substitute point sources;  $j = 1$  with door,  $j = 2,3$  without door;
- Side 4: 6 substitute point sources;  $j = 1$  to 5 identical envelope segments,  $j = 6$  for openings;
- Side 5: 15 substitute point sources;  $j = 1$  to 5 identical roof segments with light glass elements,  $j = 6$  to 15 identical roof segments without glass.